

# Control System

Note: This section was determined through reverse-engineering by Ryan and is pending confirmation.

The control system follows basic [PID theory](#), but has two additional parameters called hysteresis (H) and windup (W). The hysteresis essentially creates a deadband. If the error is below the hysteresis level, the error can be assumed as zero, and thus no corrective action is required. The windup term acts to limit the integral portion of the PID controller. If the integral value is above the windup level, it will be truncated to the windup value. Therefore, the integral can never increase or decrease infinitely because it will always be capped by the windup.

Now that we have explained the P, I, D, W, and H parameters of the control system, we're going to discuss the basic functions of the control system. Below is a simple linear algebra equation that represents our submarine's controls.

$$MC = F$$
 In  $\text{\ref{eq:control}}$ , parameter  $M$  is the maximum available force each thruster can apply on the submarine and parameter  $C$  is the thruster control signal (Note that this parameter is normalized and within the bounds  $[-1,1]$ ). By multiplying the total available force of a thruster by the command signal, we can represent the force on the submarine by the thruster as parameter  $F$ .

## Thruster Force

Let's first take a closer look at parameter  $M$  in ( $\text{\ref{eq:control}}$ ). All of our thrusters are identical, which means the total force that they can output is the same. However, the position and orientation of each thruster changes how much force it can output along the X, Y, Z, and rotational axes.

By breaking down forces into translational forces and rotational forces, it can be seen that each thruster will cause translational movement in the submarine in the form of moving forward, strafing, or diving and rotational movement in the form of pitching, rolling, or yawing. Therefore, it is useful to represent a thruster as a combination of all six forces.

$$\text{Thruster} = \begin{bmatrix} F_x \\ F_y \\ F_z \\ M_r \\ M_p \\ M_y \end{bmatrix}$$
 where  $F_x$  is the force in the x direction (forward),  $F_y$  is the force in the y direction (strafe),  $F_z$  is the force in the z direction (dive),  $M_y$  is the yaw moment (the tendency to cause the submarine to yaw),  $M_p$  is the pitch moment, and  $M_r$  is the roll moment.

We can therefore express the parameter  $M$  in ( $\text{\ref{eq:control}}$ ) as a matrix of each of the thruster forces and moments

$$M = \begin{bmatrix} F_{1,x} & F_{2,x} & \dots & F_{n,x} \\ F_{1,y} & F_{2,y} & \dots & F_{n,y} \\ F_{1,z} & F_{2,z} & \dots & F_{n,z} \\ M_{1,r} & M_{2,r} & \dots & M_{n,r} \\ M_{1,p} & M_{2,p} & \dots & M_{n,p} \\ M_{1,y} & M_{2,y} & \dots & M_{n,y} \end{bmatrix}$$

where moments are calculated by multiplying position by force.

## Control Command

The parameter  $C$  in ([eq:control](#)) is fairly straightforward. This parameter contains a single value bounded by  $[-1,1]$  to scale each thruster force by. Therefore,  $C$  can be represented as

$$C = \begin{bmatrix} C_1 & C_2 & \dots & C_n \end{bmatrix}$$
 where  $C_x$  represents the scale factor for thruster  $x$ . Take note that conceptually, it is easy to differentiate translational and rotational goals

$$C = C_t + C_r$$
 where  $C_t$  is the translational control signal and  $C_r$  is the rotational control signal.

## Total Force

By substituting ([eq:control:M](#)) and ([eq:control:C](#)) into ([eq:control](#)), it can be seen that

$$\begin{bmatrix} F_{1,x} & F_{2,x} & \dots & F_{n,x} \\ F_{1,y} & F_{2,y} & \dots & F_{n,y} \\ F_{1,z} & F_{2,z} & \dots & F_{n,z} \\ M_{1,r} & M_{2,r} & \dots & M_{n,r} \\ M_{1,p} & M_{2,p} & \dots & M_{n,p} \\ M_{1,y} & M_{2,y} & \dots & M_{n,y} \end{bmatrix} \begin{bmatrix} C_1 & C_2 & \dots & C_n \end{bmatrix} = \begin{bmatrix} F_x \\ F_y \\ F_z \\ M_r \\ M_p \\ M_y \end{bmatrix}$$
 Therefore,  $F$  is also a vector with 6 elements in it. Each element of  $F$  is the summation of each of the rows of  $M$  multiplied by the weights in  $C$ .

## Solving the Equation

Now that all of the parameters of ([eq:control](#)) have been defined, we can use it to find our control. Notice that there are two knowns within the system, both  $M$  and  $F$  can be analytically determined.  $M$  can be found by measuring the position and orientation of each thruster.  $F$  results from the desired position of the sub.  $F$  can be modified to cause the sub to move and rotate at specific speeds. It can be derived directly from the desired state and the current state of the submarine. The derivation of  $F$  will be added in the future. For now, take  $F$  as our parameter to variate.

Because both  $F$  and  $M$  are known, ([eq:control](#)) can be solved for  $C$

$$C = M^{-1}F$$
 Therefore, to solve for the control messages to send to the thruster, the inverted matrix  $M^{-1}$  can be multiplied into the variable parameter  $F$ . The control packet  $C$  can then be sent to the thruster controller to result in the desired movement and the cycle can be completed.

Also note that the following simplification can be made to solve for  $C_r$  and  $C_t$  from ([eq:c:simplification](#)) by setting  $F_a$  or  $M_a$  to zero in  $F$

$$C_t = M^{-1} \begin{bmatrix} F_x \\ F_y \\ F_z \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

$$C_r = M^{-1} \begin{bmatrix} 0 \\ 0 \\ 0 \\ M_r \\ M_p \\ M_y \end{bmatrix}$$

# Control System Notes

1. When tuning pitch and roll tune PID params while the sub is moving. This is because we only currently care about keeping the sub level while moving.

From:

<https://robosub.eecs.wsu.edu/wiki/> - **Palouse RoboSub Technical Documentation**

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